

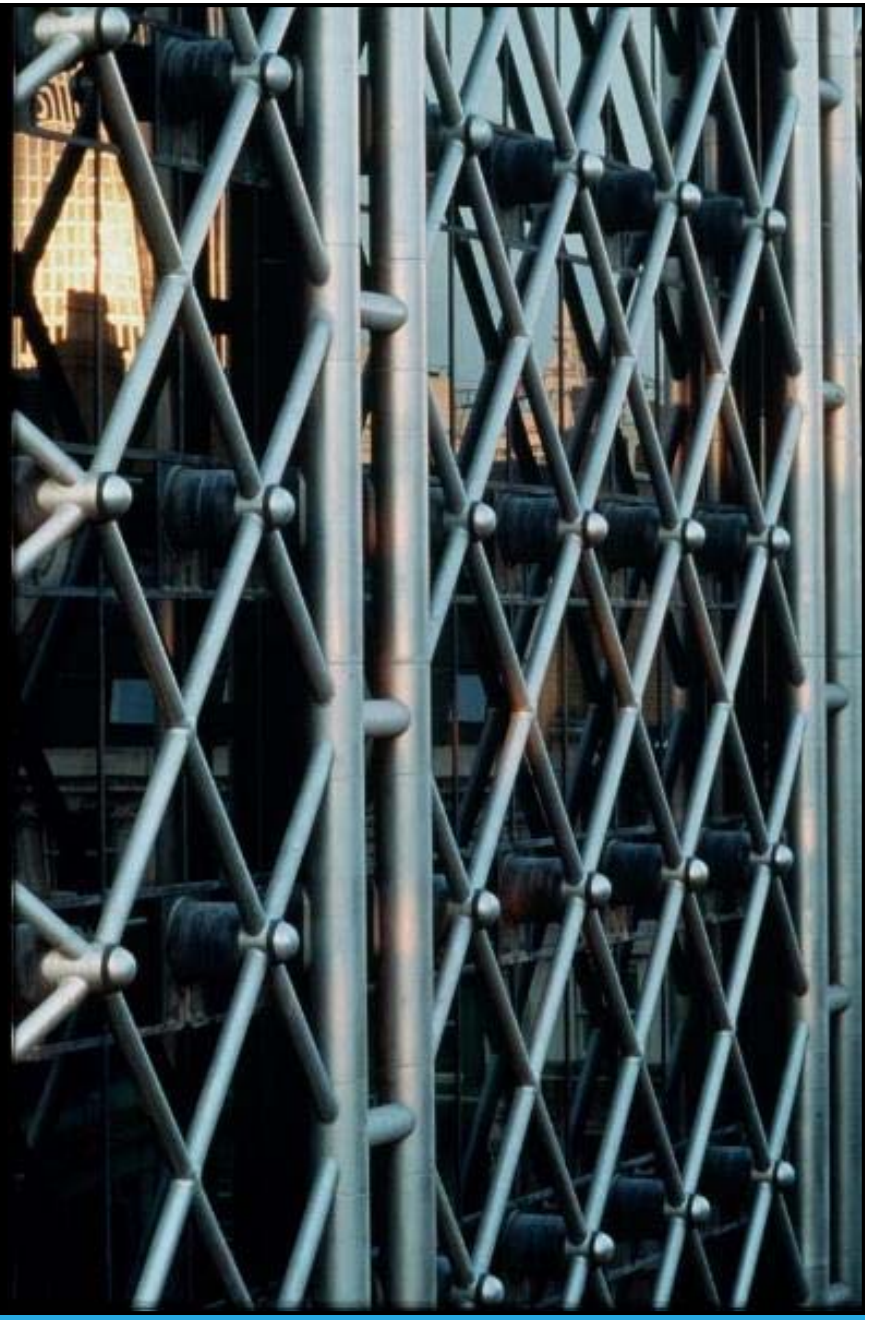
# Design and evaluation of new and existing stainless steel structures in Europe

Graham Gedge, Arup Materials

*“Surely, there is a better way?”*



*“There is a better way – find it”*























# EN1993-1-4 Annex A

## Selection of materials and durability





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# Annex A 2015 - Significant changes

- The Annex is “**Normative**”
- Introduces concepts of Corrosion Resistance Factor – **CRF** and Corrosion Resistance Class - **CRC**

**Table A.1: Determination of Corrosion Resistance Factor CRF =  $F_1 + F_2 + F_3$**

F <sub>1</sub> Risk of exposure to chlorides from salt water or deicing salts		
NOTE: M is distance from the sea and S is distance from roads with deicing salts.		
1	Internally controlled environment	
0	Low risk of exposure	M > 10 km or S > 0,1 km
-3	Medium risk of exposure	1 km < M ≤ 10 km or 0,01 km < S ≤ 0,1 km
-7	High risk of exposure	0,25 km < M ≤ 1 km or S ≤ 0,01 km
-10	Very high risk of exposure	Road tunnels where deicing salt is used or where vehicles might carry deicing salts into the tunnel
-10	Very high risk of exposure	M ≤ 0,25 km North Sea coast of Germany and all Baltic coastal areas
-15	Very high risk of exposure	M ≤ 0,25 km Atlantic coast line of Portugal, Spain and France. English Channel and North Sea Coastline of UK, France, Belgium, Netherlands and Southern Sweden. All other coastal areas of UK, Norway, Denmark and Ireland. Mediterranean Coast
F <sub>2</sub> Risk of exposure to sulfur dioxide		
For European coastal environments the sulfur dioxide concentration is usually low. For inland environments the sulfur dioxide concentration is either low or medium. The high classification is unusual and associated with particularly heavy industrial locations or specific environments such as road tunnels. Sulfur dioxide concentration may be evaluated according to the method in ISO 9225.		
0	Low risk of exposure	< 10 µg/m <sup>3</sup> average gas concentration
-5	Medium risk of exposure	10 - 90 µg/m <sup>3</sup> average gas concentration
-10	High risk of exposure	90 - 250 µg/m <sup>3</sup> average gas concentration
F <sub>3</sub> Cleaning regime or exposure to washing by rain (if F <sub>1</sub> +F <sub>2</sub> ≥ 0, then F <sub>3</sub> = 0)		
0	Fully exposed to washing by rain	
-2	Specified cleaning regime	
-7	No washing by rain or No specified cleaning	
If the component is to be regularly inspected for any signs of corrosion and cleaned, this should be made clear to the user in written form. The inspection, cleaning method and frequency should be specified. The more frequently cleaning is carried out, the greater the benefit. The frequency should not be less than every 3 months. Where cleaning is specified it should apply to all parts of the structure, and not just those easily accessible and visible		

## EN 1993-1-4 Annex A [normative] Selection of materials and durability

**Table A.2: Determination of Corrosion Resistance Class CRC**


Corrosion Resistance Factor (CRF)	Corrosion Resistance Class (CRC)
CRF = 1	I
0 ≥ CRF > -7	II
-7 ≥ CRF > -15	III
-15 ≥ CRF > -20	IV
CRF < -20	V

**Table A.3: Grades in each Corrosion Resistance Class CRC**

Corrosion resistance class CRC				
I	II	III	IV	V
1.4003	1.4301	1.4401	1.4439	1.4565
1.4016	1.4307	1.4404	1.4462	1.4529
1.4512	1.4311	1.4435	1.4539	1.4547
	1.4541	1.4571		1.4410
	1.4318	1.4429		1.4501
	1.4306	1.4432		1.4507
	1.4567	1.4162		
	1.4482	1.4662		
		1.4362		
		1.4062		
		1.4578		

A grade from a higher class may be used in place of the class indicated by the CRF.  
NOTE: The corrosion resistant classes are only intended for use with this grade selection procedure and are only applicable to structural applications.

### A.3 Swimming pool environments

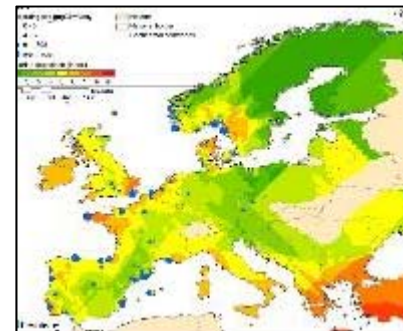
- (1) To address the risk of stress corrosion cracking (SCC) in pool atmospheres, only the steel grades given in Table A.4 shall be used for load bearing parts exposed to atmospheres above indoor swimming pools. 



# CRF and CRC Evaluation

# Chloride exposure F1

- Direct operating experience
- Exposure test site data in Europe
- Chloride mapping data
- Chloride deposition data



# Example Specification

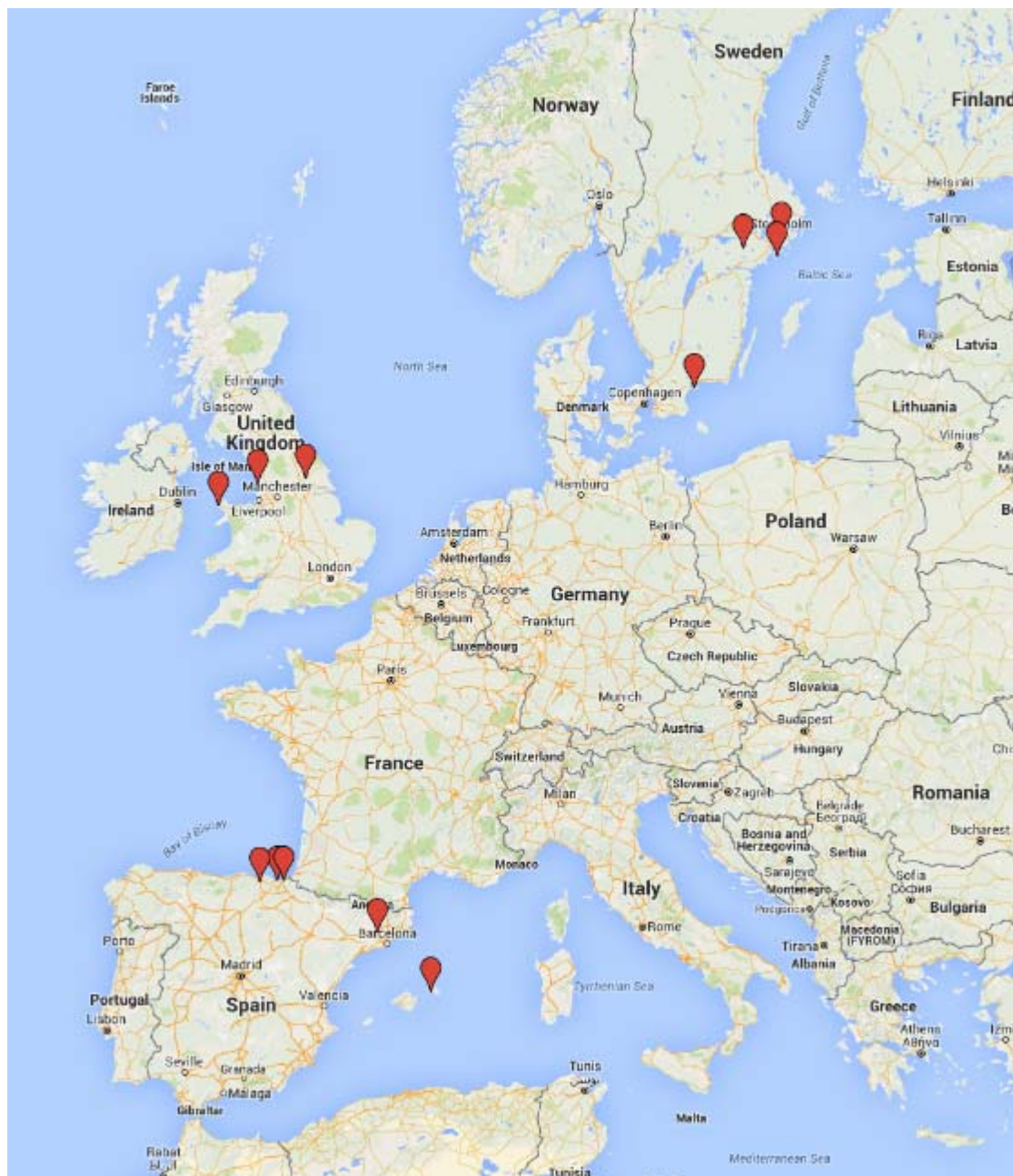
$f_y = 200 \text{ N/mm}^{-2}$  CRC II (Austenitic with no Mo)

$f_y = 450 \text{ N/mm}^{-2}$  CRC III (Lean duplex)

The final choice of alloy is for the supplier



# Annex A – real structures



Structure name	Location	Year of construction
<b>Sölvesborg Pedestrian and Cycle Bridge</b>	Solvesborg, Sweden	2013
<b>Orrhammarvägen Bridge</b>	Flen, Sweden	2009
<b>Sicklauddsbron</b>	Stockholm, Sweden	2002
<b>Nynashamn road bridge</b>	Nynashamn, Sweden	2011
<b>Millennium Bridge</b>	York, United Kingdom	2000
<b>Blackpool seafront (various elements)</b>	Blackpool, United Kingdom	Circa 2000-2010
<b>Celtic Gateway Bridge</b>	Holyhead, United Kingdom	2006
<b>Sant Fruitós Bridge</b>	Manresa, Spain	2009
<b>Zumaia footbridge</b>	Zumaia, Spain	2008
<b>Anorga bridge</b>	San Sebastian, Spain	2011
<b>Puerto Arrupe</b>	Bilbao, Spain	2003
<b>Cala Galdana bridge</b>	Menorca, Spain	2005



Various foreshore elements, Blackpool, England  
Various architects, 2002—





Various foreshore elements, Blackpool, England  
Various architects, 2002—



Various foreshore elements, Blackpool, England  
Various architects, 2002—





Various foreshore elements, Blackpool, England  
Various architects, 2002—





Celtic Gateway Bridge, Holyhead, Wales  
2006. Alloy 1.4362 for the structure



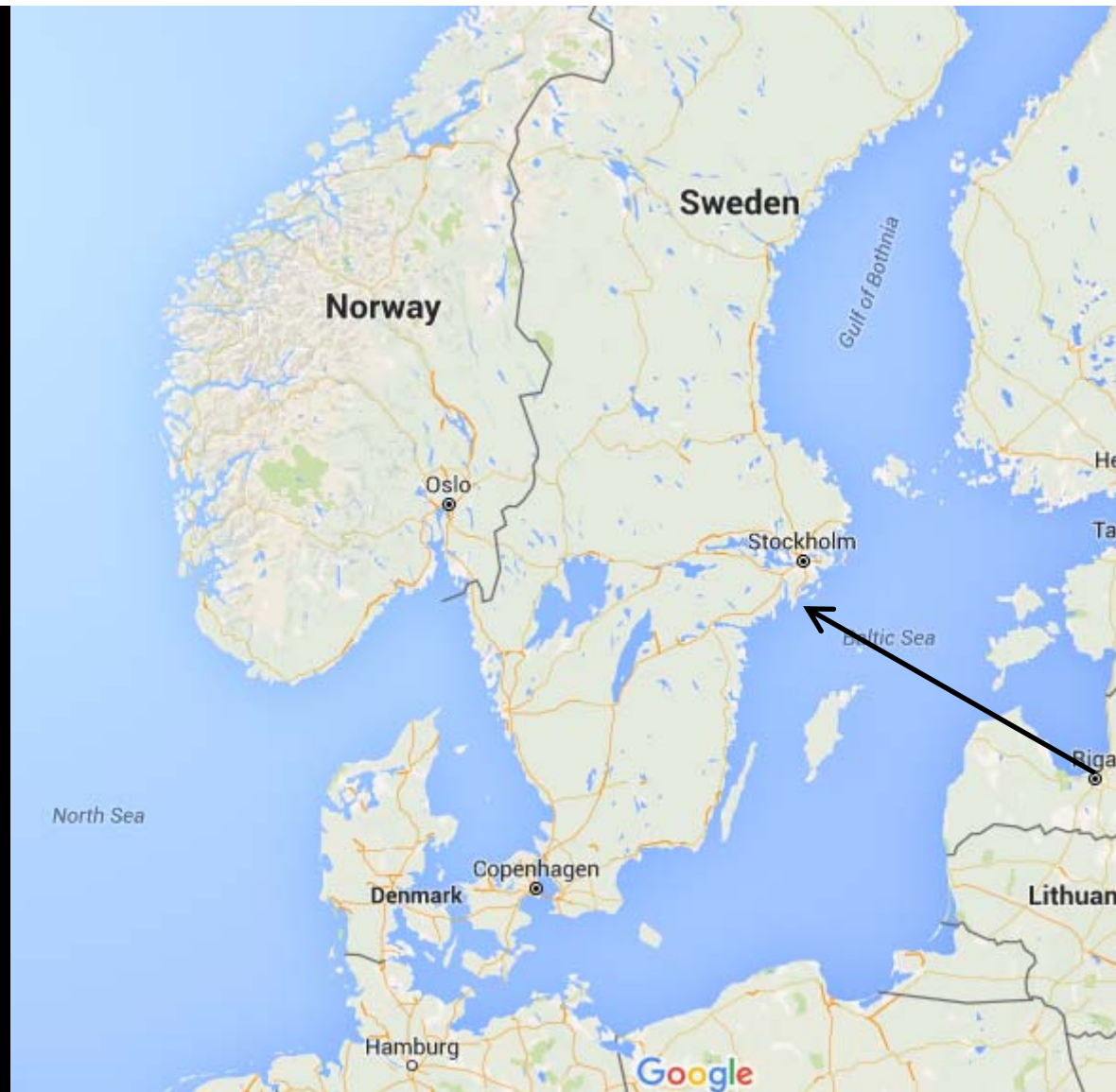
Celtic Gateway Bridge, Holyhead, Wales  
2006. Alloy 1.4362 for the structure





Celtic Gateway Bridge, Holyhead, Wales  
2006. Alloy 1.4362 for the structure





Nynashamn road bridge, Nynashhamn, Sweden  
2011. Alloy 1.4162



Nynashamn road bridge, Nynashamn, Sweden  
2011. Alloy 1.4162



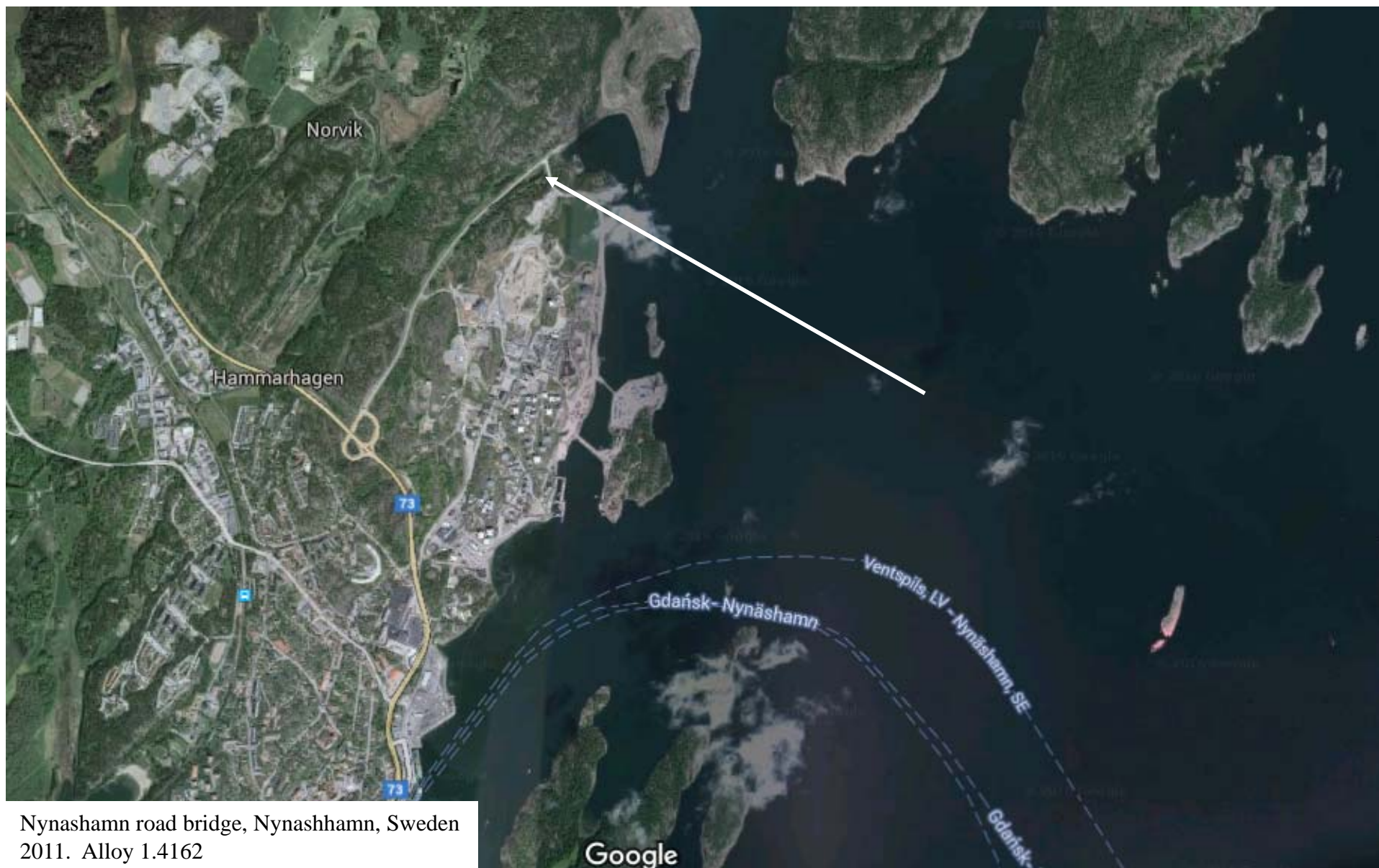


Nynashamn road bridge, Nynashhamn, Sweden  
2011. Alloy 1.4162





Nynashamn road bridge, Nynashhamn, Sweden  
2011. Alloy 1.4162



Nynashamn road bridge, Nynashhamn, Sweden  
2011. Alloy 1.4162

# Lessons learned?

- Annex A is consistent with performance
- Lean duplex outperform assumptions
- Requires better guidance on assessing the environment



