



The strength of stainless steel fillet welds using GMAW

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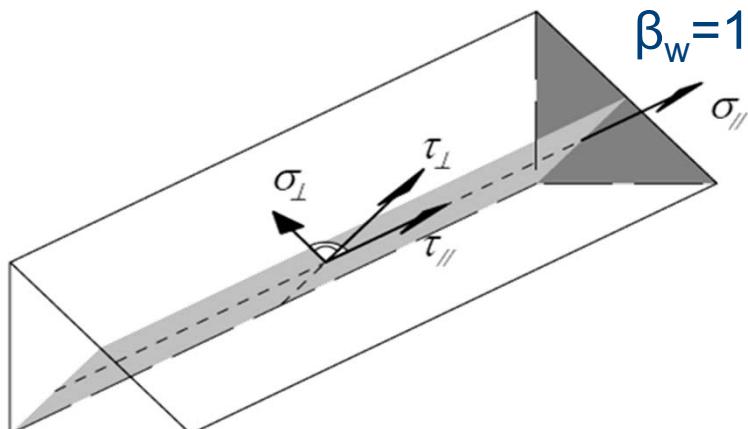
KU Leuven, Belgium



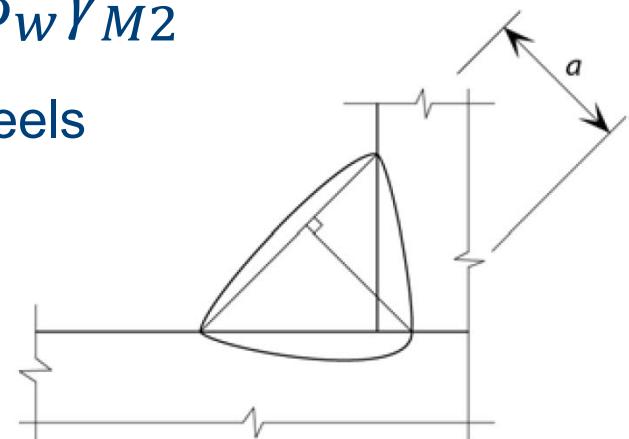
Objective

- Design of a weld based on Von Mises
 - σ_{\perp} The normal stress perpendicular to the critical plane of the throat
 - σ_{\parallel} The normal stress parallel to the axis of the weld (neglected)
 - τ_{\perp} The shear stress in the critical plane of the throat perpendicular to the weld axis
 - τ_{\parallel} The shear stress in the critical plane of the throat parallel to the weld axis

$$\sqrt{\sigma_{\perp}^2 + 3(\tau_{\perp}^2 + \tau_{\parallel}^2)} \leq \frac{f_u}{\beta_w \gamma_{M2}}$$



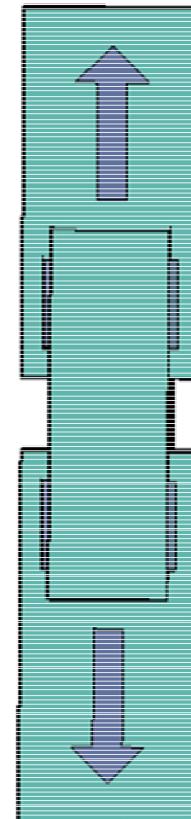
$\beta_w = 1$ for all stainless steels



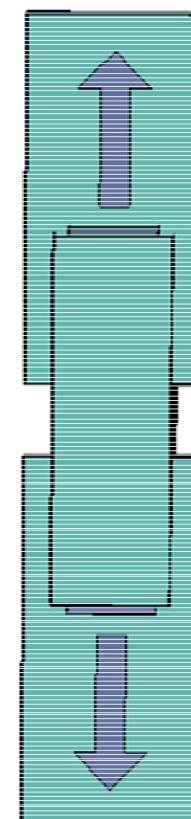
Test program

- 3 grades
 - EN 1.4062 Lean duplex (2202)
 - EN 1.4404 Austenitic (316L)
 - EN 1.4307 Austenitic (304L)
- 2 loading conditions
 - Longitudinal
 - Transverse
- 1 welding process
 - Manual GMAW
 - Overalloyed consumables
 - Matched mechanical strength
- Coupons base material, microstructure & hardness

Longitudinal

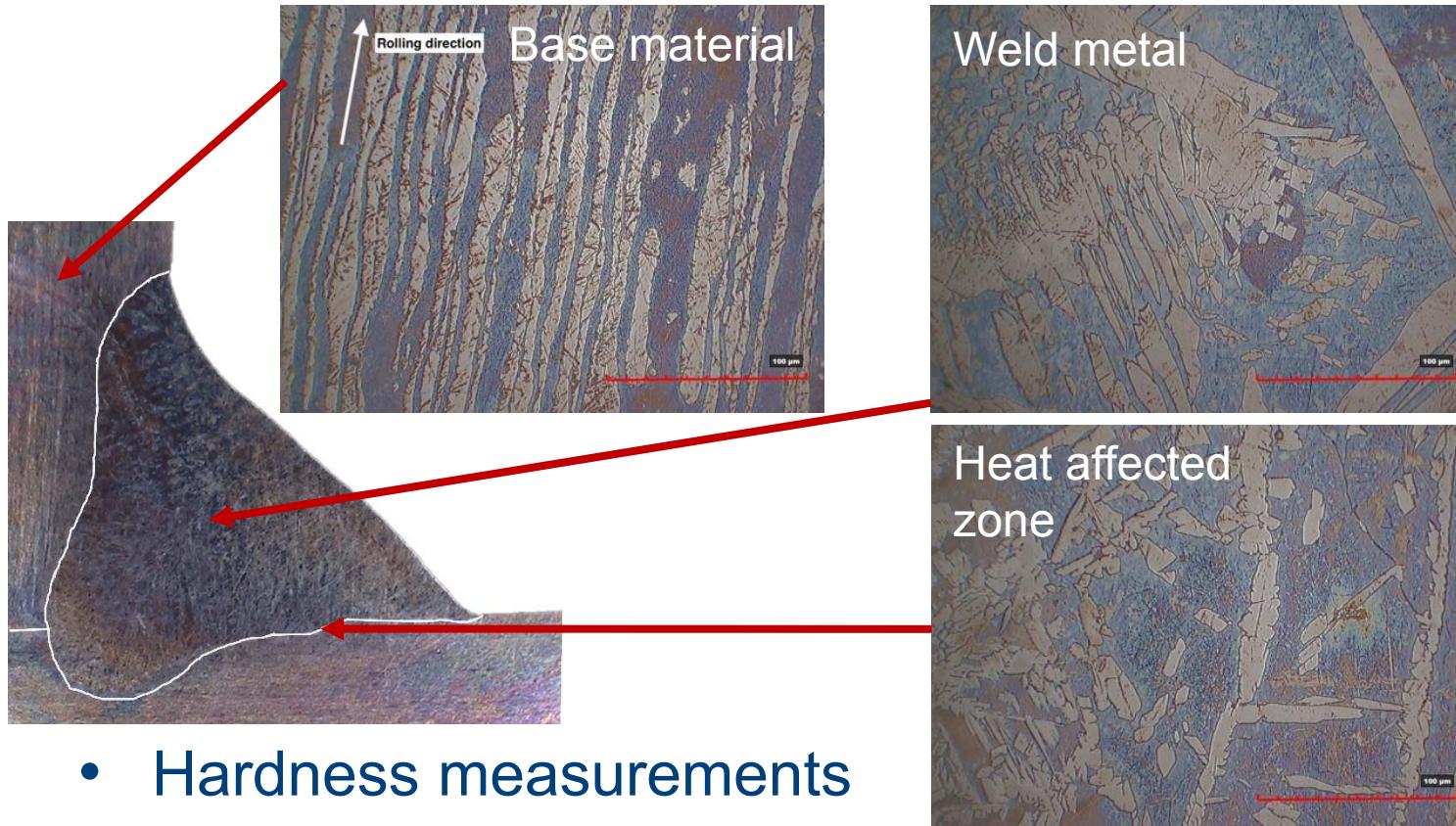


Transverse

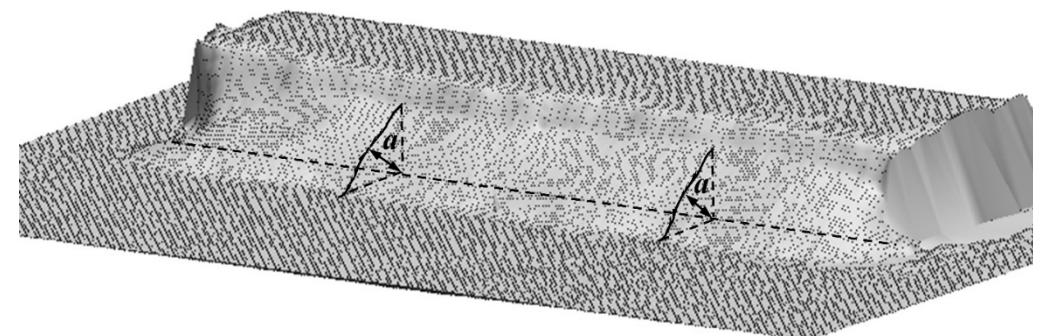
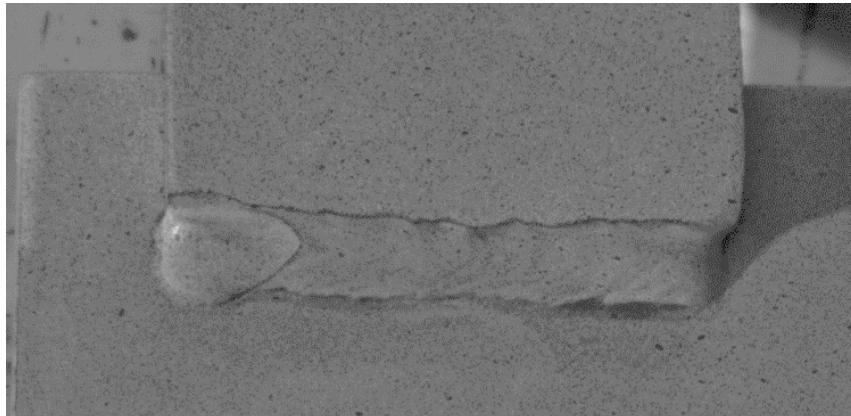


Inspection of the welds

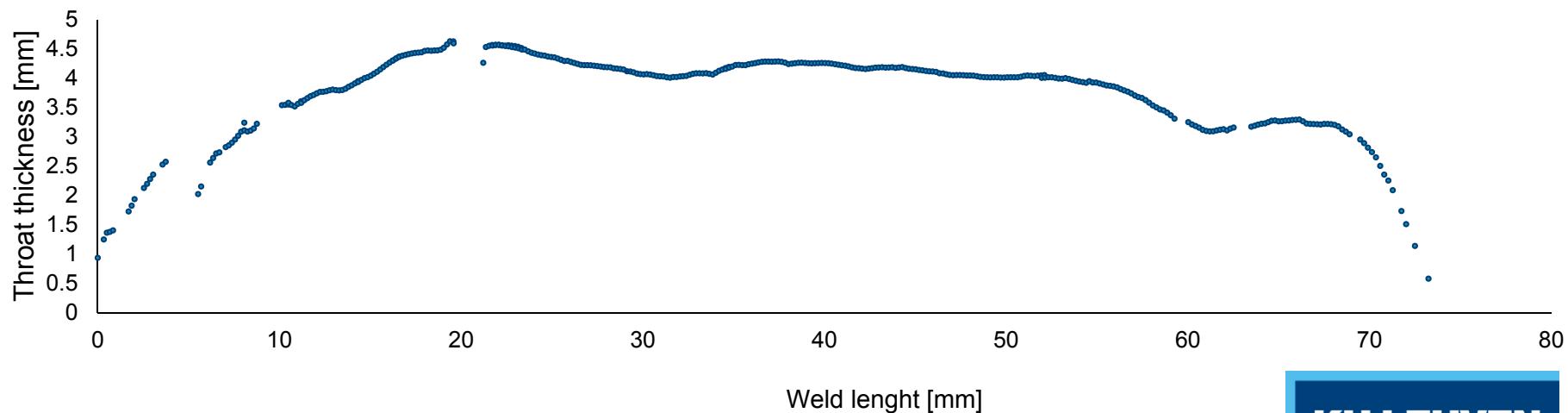
- Manual Gas Metal Arc Welding (GMAW)
- Macroscopic and microscopic investigation



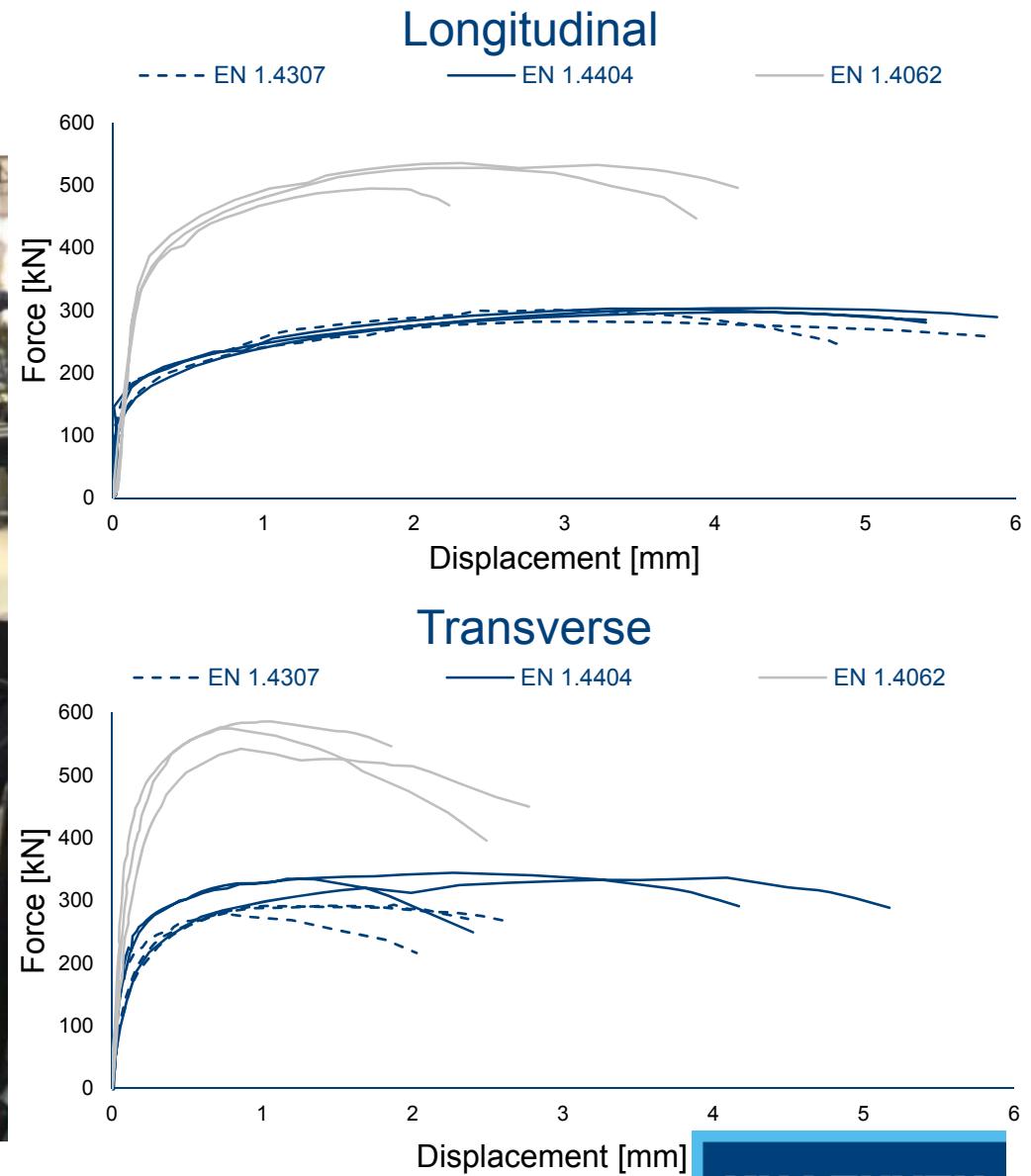
Initial geometry of the weld



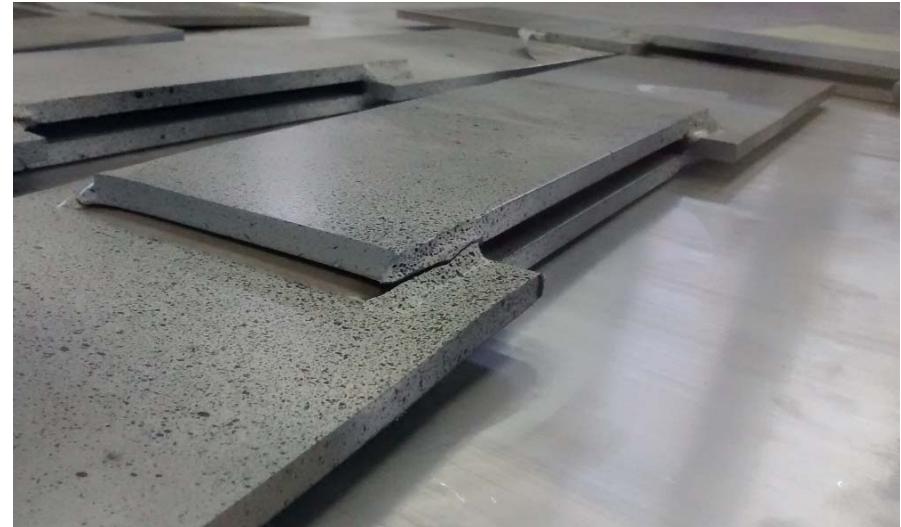
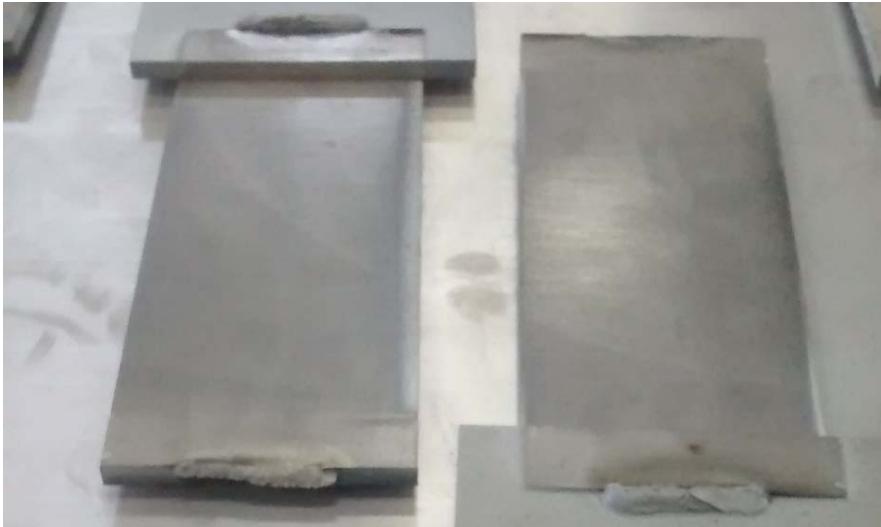
Cross-section weld



Test results

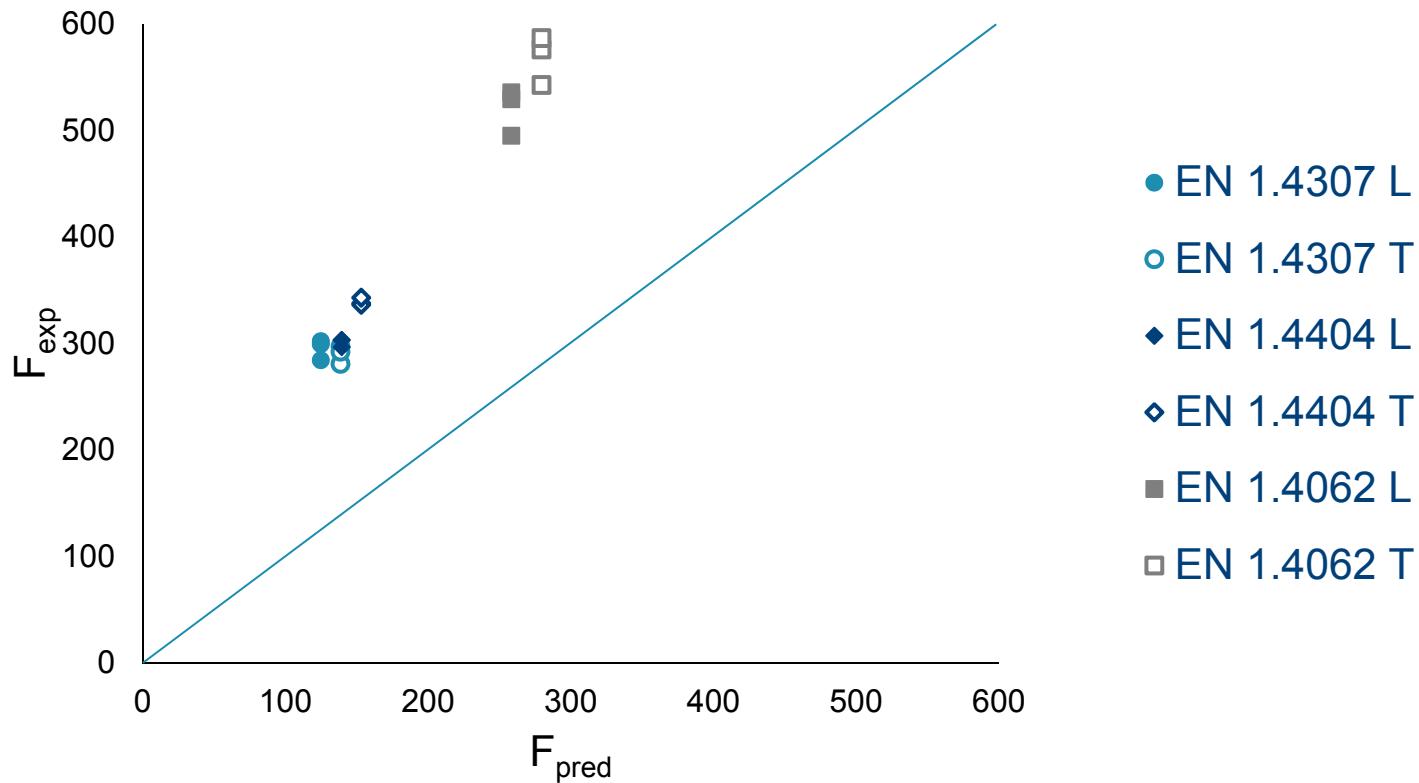


Test results



Assessment of the design rules

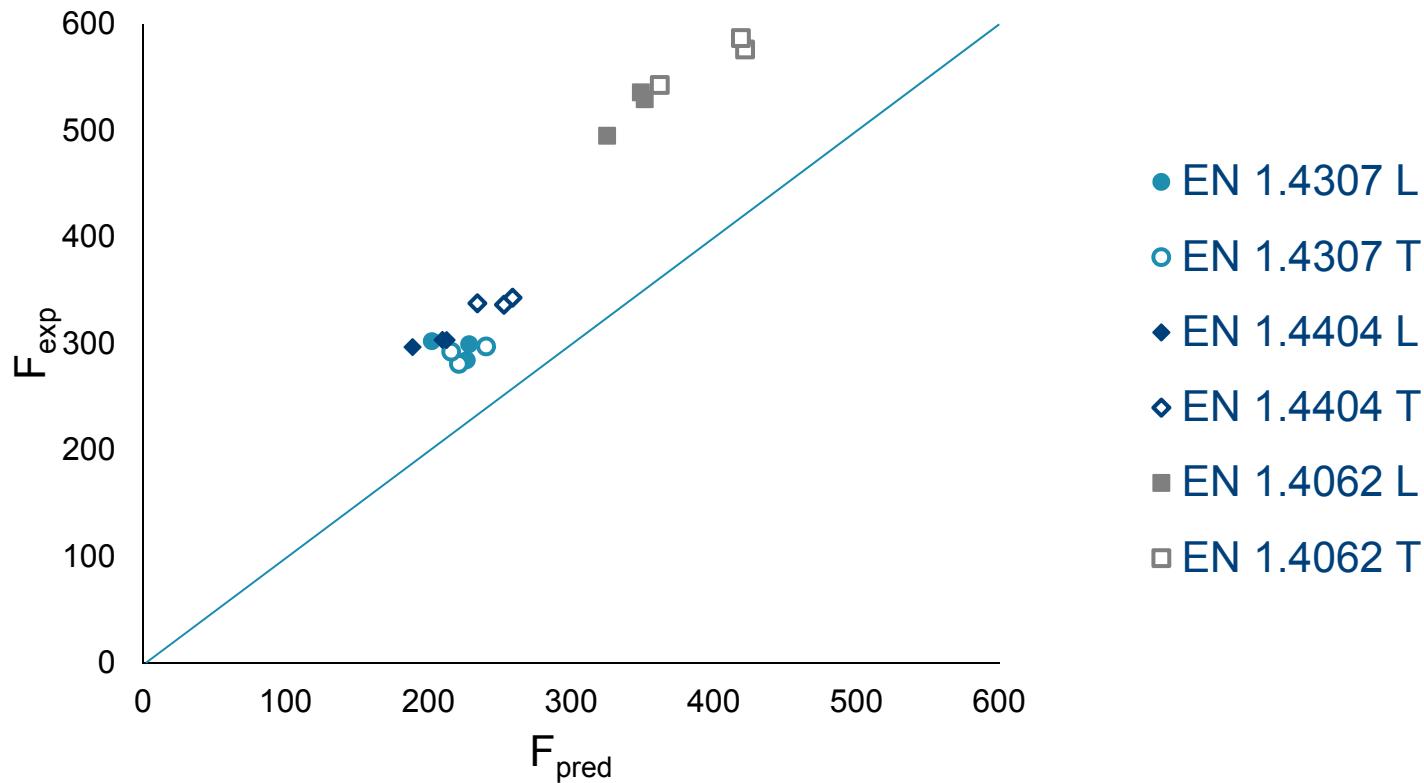
- Using design values
 - $A_1 = a_{nom} * (l_{nom} - 2a_{nom})$



Assessment of the design rules

- Using measured geometry

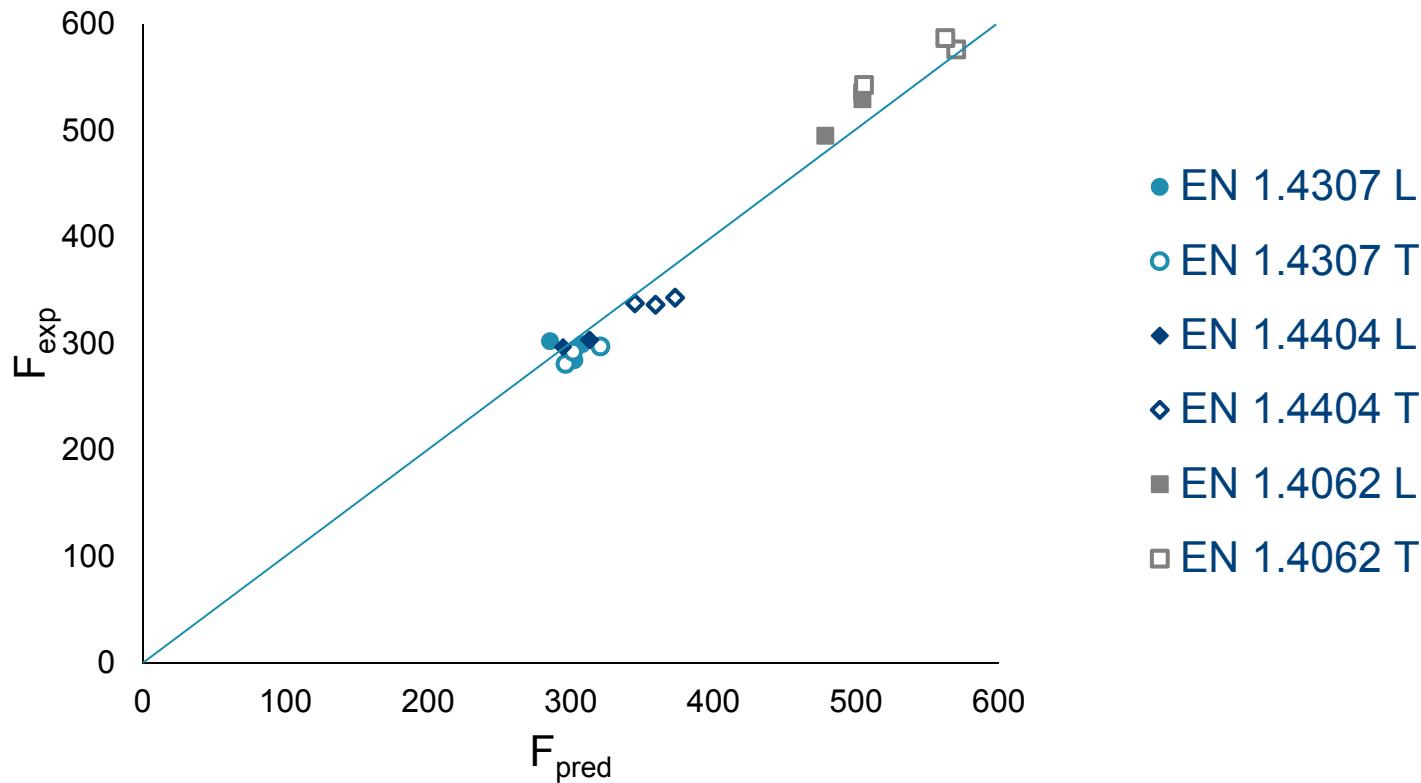
- $A_2 = a_{eff} * l_{eff}$



Assessment of the design rules

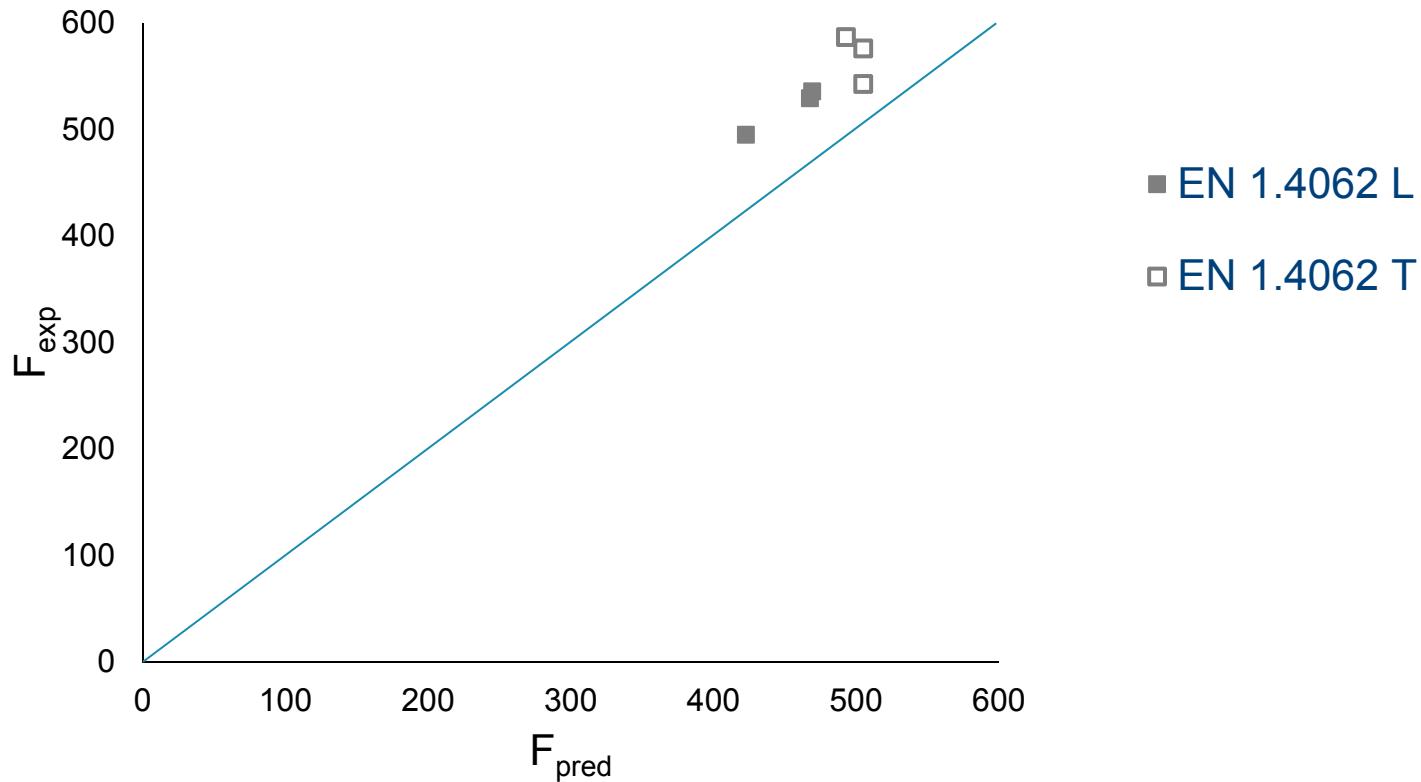
- Using the excessive penetration

- $$A_3 = a_{eff} * l_{eff} + i * (l_{eff} - 2a_{eff})$$



Assessment of the design rules

- Using the measured fracture area
 - $A_4 = A_{fracture}$



Conclusions

- The test results show that it is safe to use the current design rules in EN1993-1-8 together with the correlation factor β_w of 1, as specified in EN1993-1-4.
- The tests on duplex suggest that a lower β_w value could be possible for this material, with an average experimental-to-predicted strength ratio of 1.14, using the fracture area.
- A slightly lower ratio was found for the austenitic grades, leading to the preliminary conclusion that a correlation factor β_w of 1 is suitable for these grades.
- Currently, a campaign of 30 additional tests using various welding procedures is ongoing. The additional results will enable us to conclude on the correlation factor for duplex and austenitic stainless steel.



Thank you for your
attention

Questions?

